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507 SOBA

TAJNICA: SILVA BRENCIČ 510 SOBA

PIŠEMO Z YOLOZUIJA K1 K2

YOLOZUIJ OBSEGA S UPRAŠANJ

2 TOČI TA UPRAŠANJE

TRI VRSTE UPRAŠANJ: LAHKA, SREDNJA, TEŽKA

$$S = 2 \times L + 2 \times S + 1 \times T$$

$$2 \text{ TOČI} = 4 \times 0,5 \text{ TOČE}$$

$$5 \times 2 = 10 \text{ TOČI (MAXIMUM)}$$

ΣΑΧΟ ΟΠΡΑΥΤΙ ΙΖΠΙΤ?

ΠΙΣΕ ΣΕ 2 ΧΟΛΟΧΥΙΖΑ

$$\frac{k_1 + k_2}{2} \geq 5,5 \wedge k_1 \geq 4,5 \wedge k_2 \geq 4,5 \quad \checkmark$$

ΙΖΠΙΤ ΟΠΡΑΥΤΕΝ Σ ΧΟΛΟΧΥΙΖΙ

$$k_1 = \emptyset \wedge k_2 \geq 5,5$$

$$k_1 \geq 5,5 \wedge k_2 = \emptyset$$

↑

ΠΟΤΙΤΙΥΝΑ ΟΧΕΝΑ

→

ΠΡΙΖΑΥΙΤΕ ΝΑ ΙΖΠΙΤ
ΝΑ ΧΑΤΕΡΕΜ ΠΙΣΕΤΕ
ΛΕ ΣΝΟΥ ΣΛΑΒΣΕΓΑ
ΧΟΛΟΧΥΙΖΑ

$$k_1 = 4,5 \wedge k_2 = 5,5 \rightarrow k_1$$

$$k_1 = 5 \wedge k_2 = 5 \rightarrow U = k_1 + k_2$$

$$k_1 = 7,5 \wedge k_2 = 4,5 \rightarrow \checkmark$$

$$k_1 = 2.0 \quad \wedge \quad k_2 = 2.5 \rightarrow k_1 + k_2 < 5.5 \rightarrow P + U$$

P - 17PIT 17 NALOG (60 MINUT)

U - 17PIT 18 KOMPLETNE TEORIJE $k_1 + k_2$ (60 MINUT)

$$P \geq 5.5 \quad \wedge \quad U \geq 5.5 \rightarrow \checkmark$$

REN, GLODEŽ : STROJNI ELEMENTI 1

REN, GLODEŽ : STROJNI ELEMENTI

UUD V GONILA, TORNA, ŽERKENSKA IN
VERIŽNA GONILA

ROLOFF MATEZ : MASCHINENELEMENTE

FLAŠČER, GLODEŽ, REN : ŽOBNIŠČA GONILA

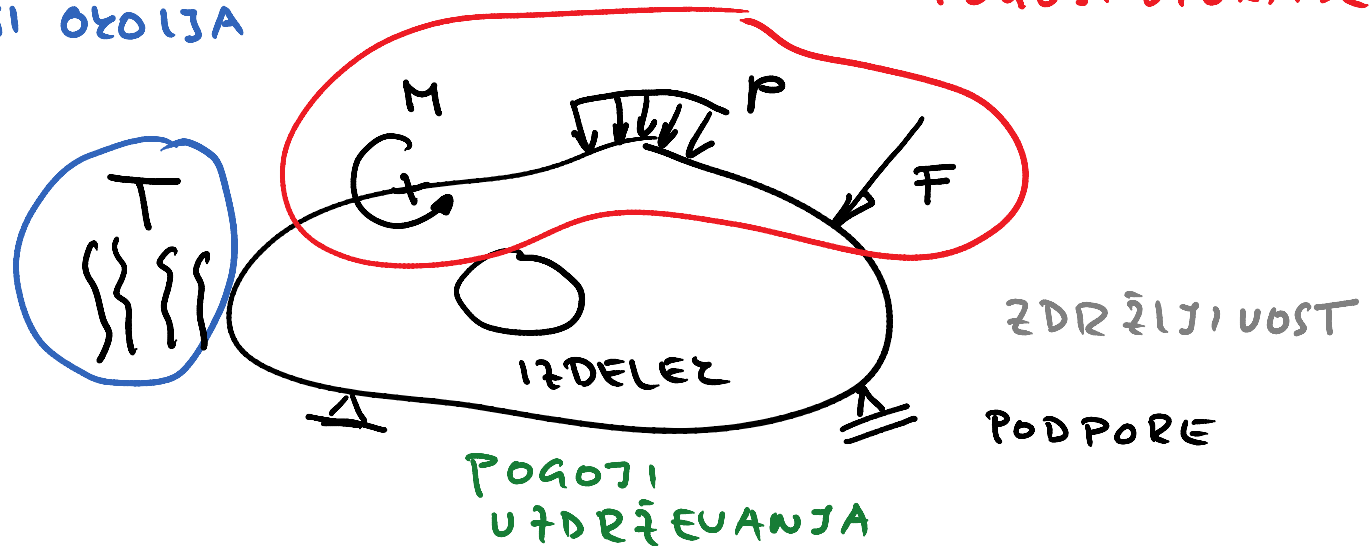
NA IZPITU MORA BITI DOSEŽENA OČENA $\geq 5,5$ V
VSAKEM PRIMERU!

VEDNO SE MORATE PRIJAVITI NA IZPIT! ZA VPIS OČENE,
ALI ZA PRISTOP K IZPITU.

UVOD

POGOJI OKOLIJA

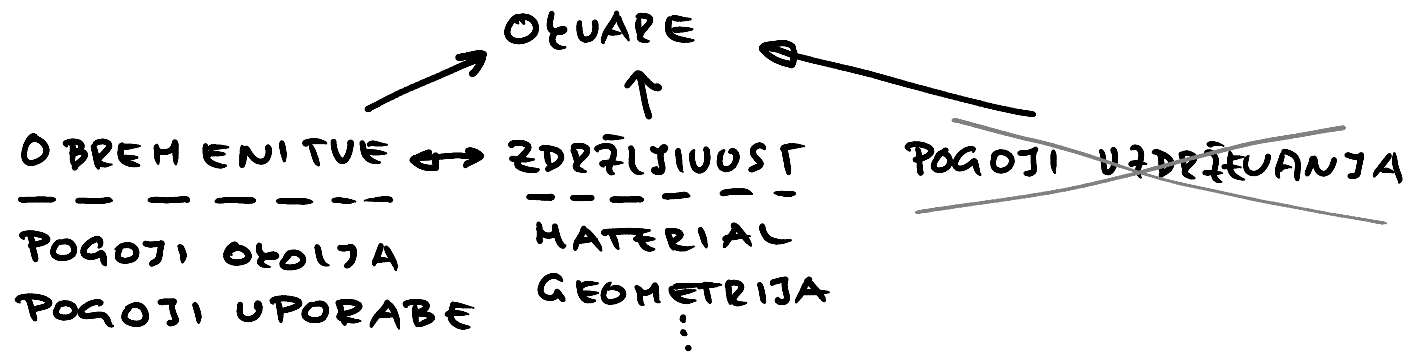
POGOJI UPORABE



F, M, p, T, \dots OBREMNITVE

FUNKCIONALNOST (1.0 ... 0.0)

OSUARA



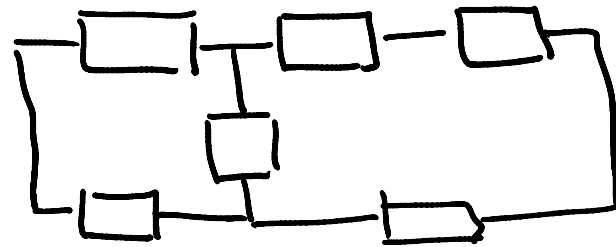
POTREBNO OPREDELITI MOŽNE VRSTE OŠUAR.

ZA USAKO VRSTO OŠUARE IZBEREMO KRITERIJ POŠKODBE.

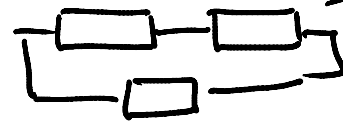
GLEDE NA KRITERIJ POŠKODBE IZBEREMO METODO VREDNOTENJA.

CILJ PREDMETA SE JE NAUČITI VREDNOTITI
RAZLIČNE STROJNE ELEMENTE!

17 DELELE



ΣΟΜΡΟΝΕΝΤΑ



ELEMENT : NAJMANJŠI
 GRADNIK, KI SE
 VEČ NE DELI
 (VIJAK, KOVICA, ŽVAR,..)

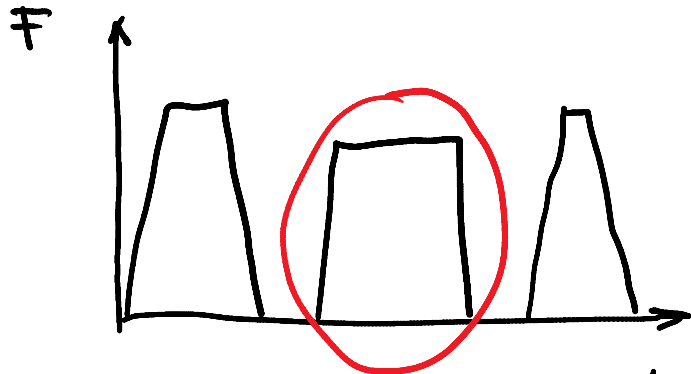
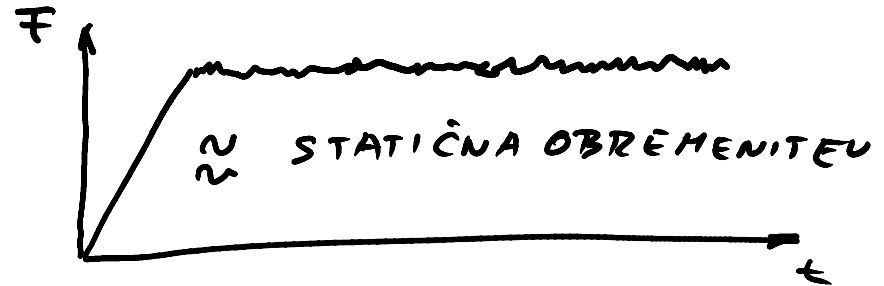
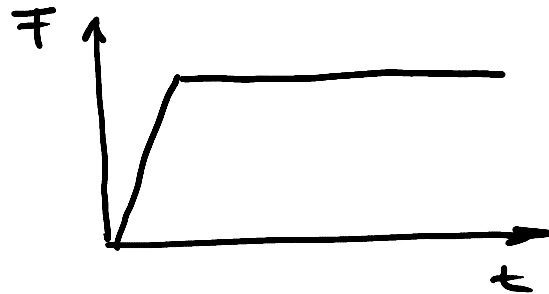
TRENUVNI

LOM - PLASTIČNI (ŽILAV MATERIAL)
 - ŽRHČI (ŽRHEČ MATERIAL)

UTRUJENOSTNI
 LOM

LEŽENJE

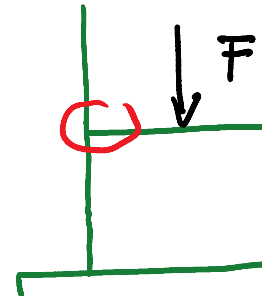
STATIČNE MATERIALNE LASTNOSTI



$N \downarrow$ KVAZI
STATIČNA

OBREHENITVENI
SIKEL

N - ŠTEVILO OBREHENITVENIH
CIKLOV



OBREHENITEV F

\downarrow
NAPETOST σ_{max}

\downarrow
ZDRŽLJIVOST

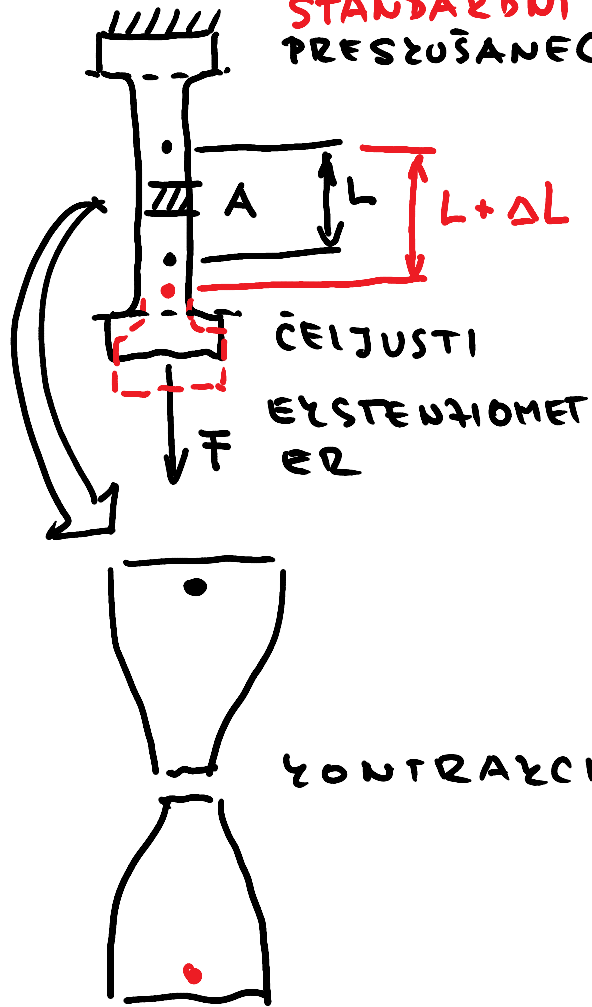
\downarrow
NAPETNA TRDNOST R_m

$$\sigma_{max} < R_m$$

VREDNOTENJE

TRQALNI STROJ

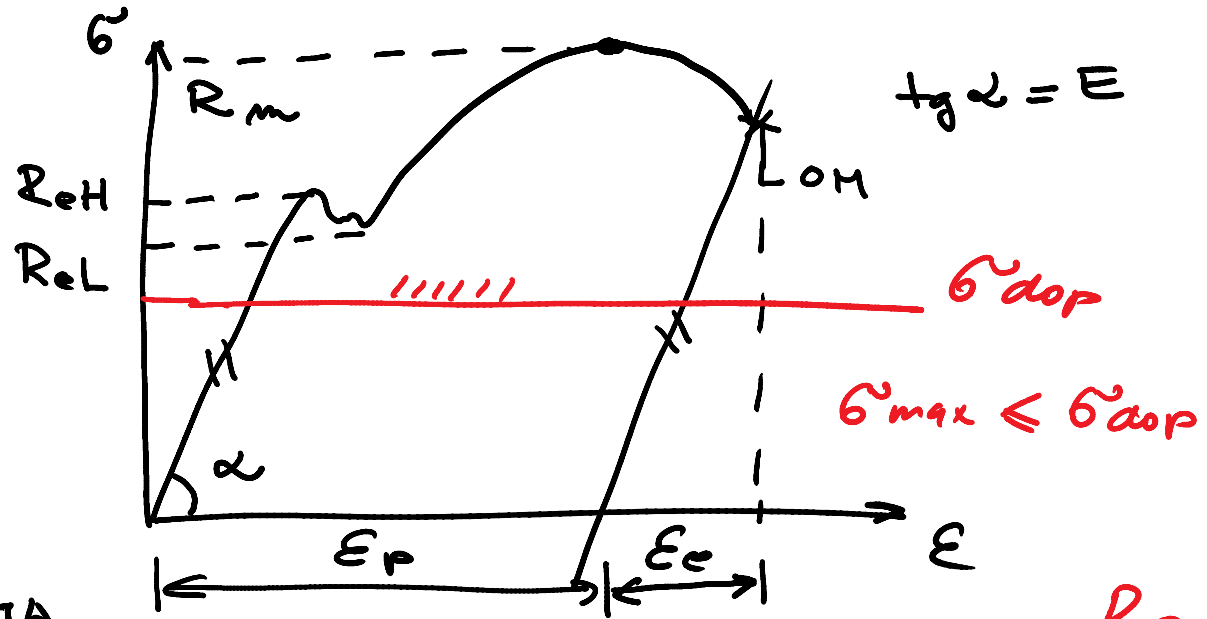
STANDARDNI
PRESUŠANEC



MATEŽNI PRESČUS

$$\epsilon = \frac{\Delta L}{L}$$

$$\sigma = \frac{F}{A} - \text{IMENSKI PRESČEŽ}$$

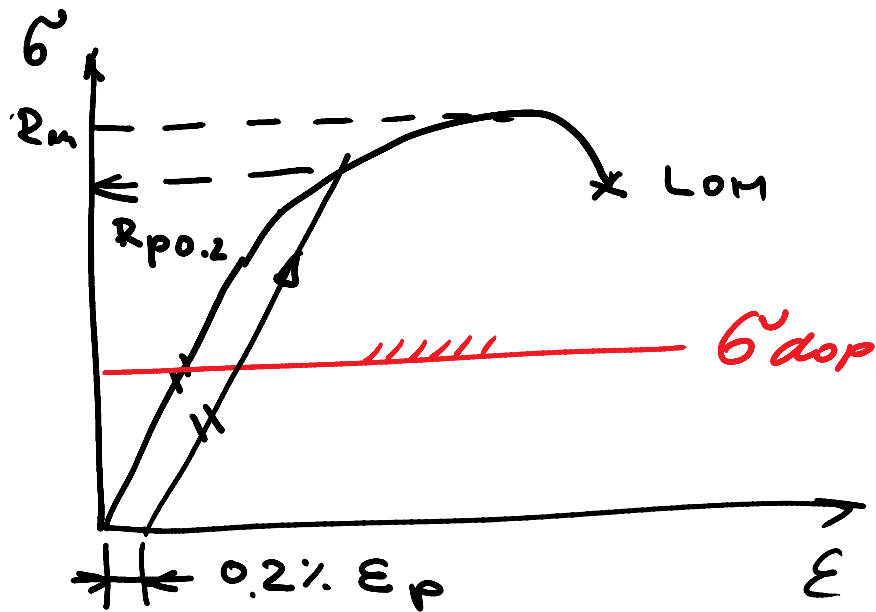


$$\epsilon = \epsilon_p + \epsilon_e$$

$$\sigma_{dop} = \frac{R_e}{\nu}$$

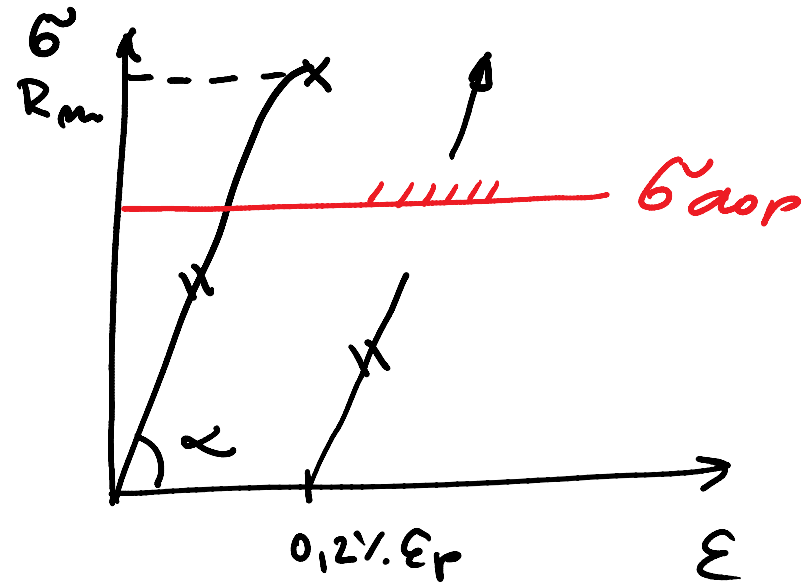
ŽILAVI MATERIALI Ž IZRAŽITO
MEJO TEČENJA

ENOSNI PRESČUS



ŽILAU MATERIAL
Z NEIŽRAŽITO
MEJO TEČENJA

$$\sigma_{dop} = \frac{R_{p0.2}}{L}$$



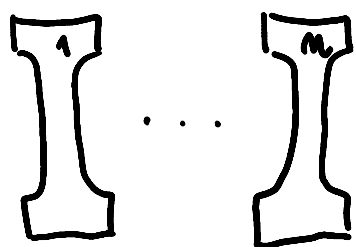
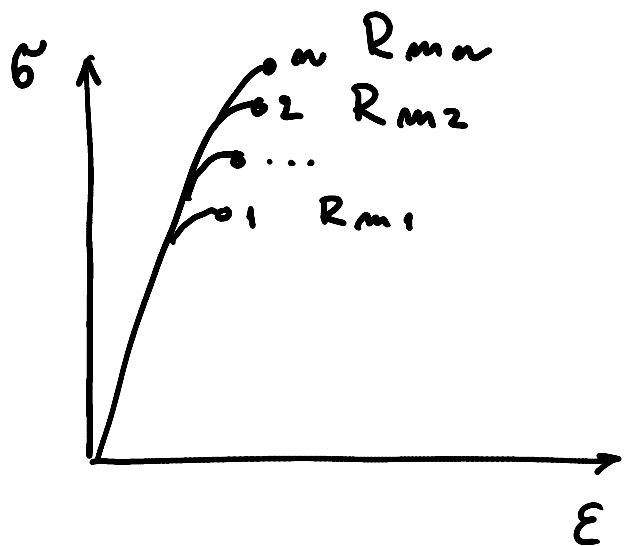
KRHKI ALI
PLASTIČNI LOM

$$\sigma_{dop} = \frac{R_m}{L}$$

KRHKI ALI
PLASTIČNI LOM!

$R_{p0.2} \rightarrow 0.2\%$ PLASTIČNE DEFORMACIJE $\epsilon_p = 0.002$

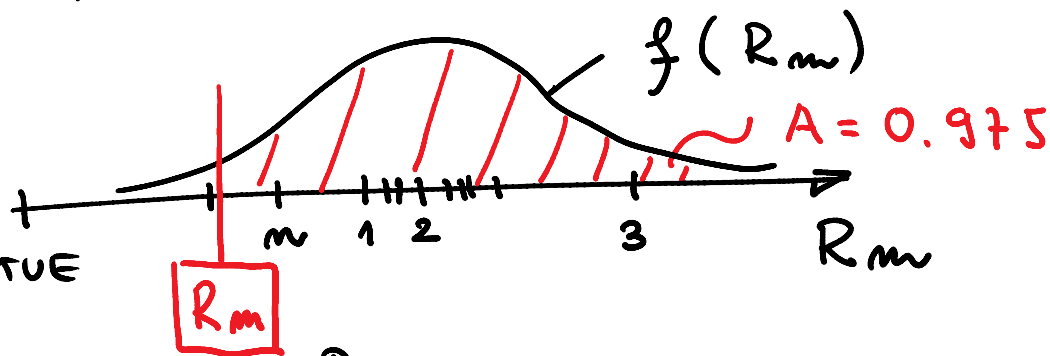
RAZTROSJI STATIČNIH MATERIALNIH LASTNOSTI



m · ŠT. ELEMENTOV
V VZORCU

POPULACIJA

R_m NAŠLIJUČNA SPREMENLJIVKA

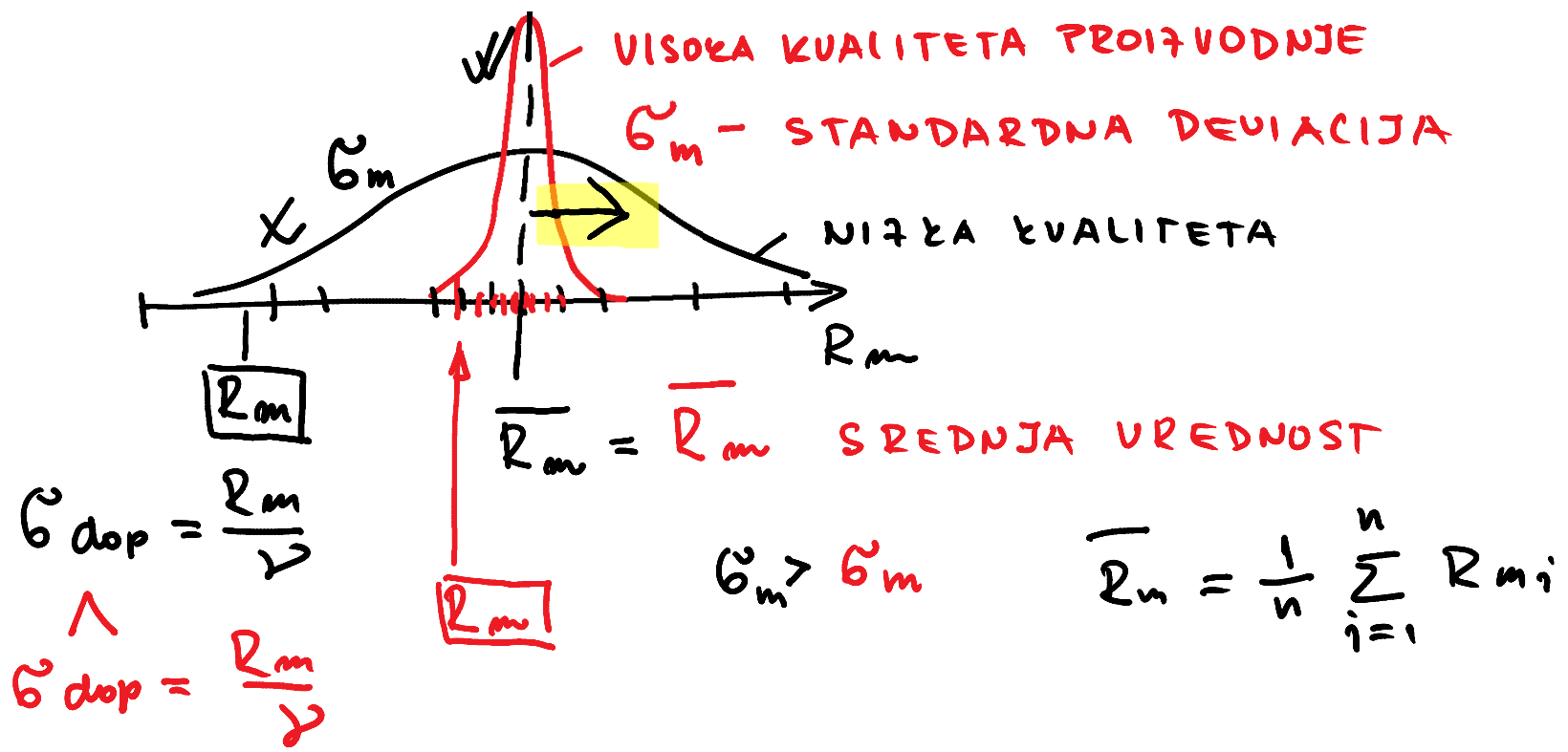


$f(R_m)$ GOSTOTA PORAZDELITVE
VERJETNOSTI

$$\int_{-\infty}^{\infty} f(R_m) dR_m = 1$$

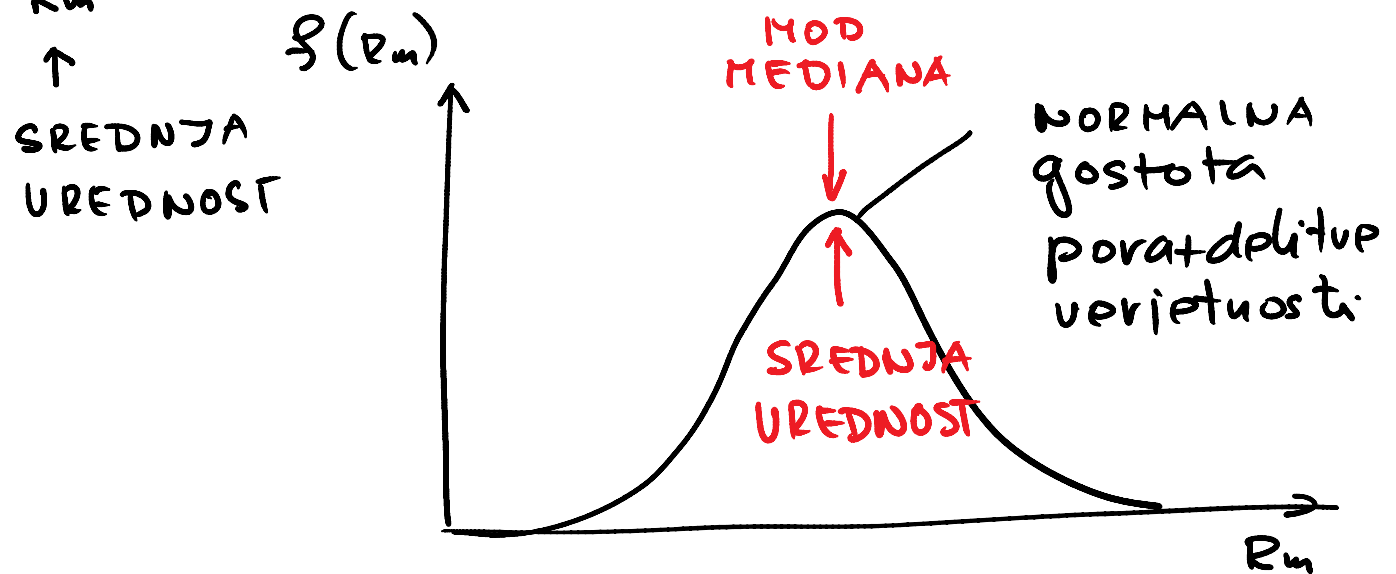
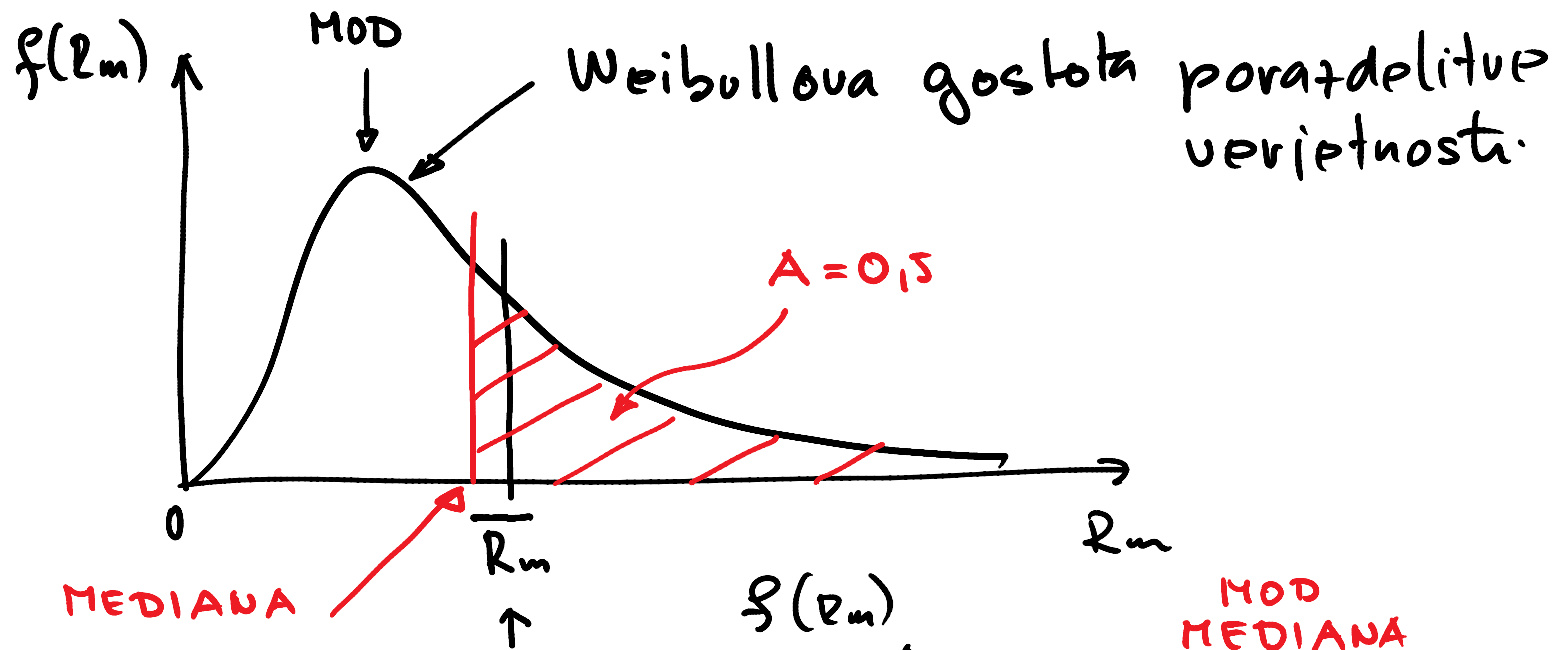
$$F(R_m) = \int_0^{R_m} f(R_m) dR_m = 1 - 0,975$$

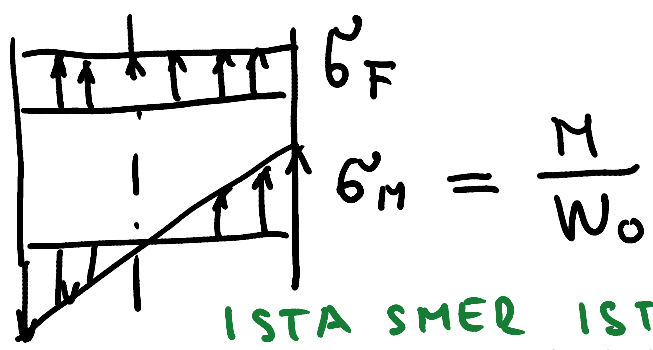
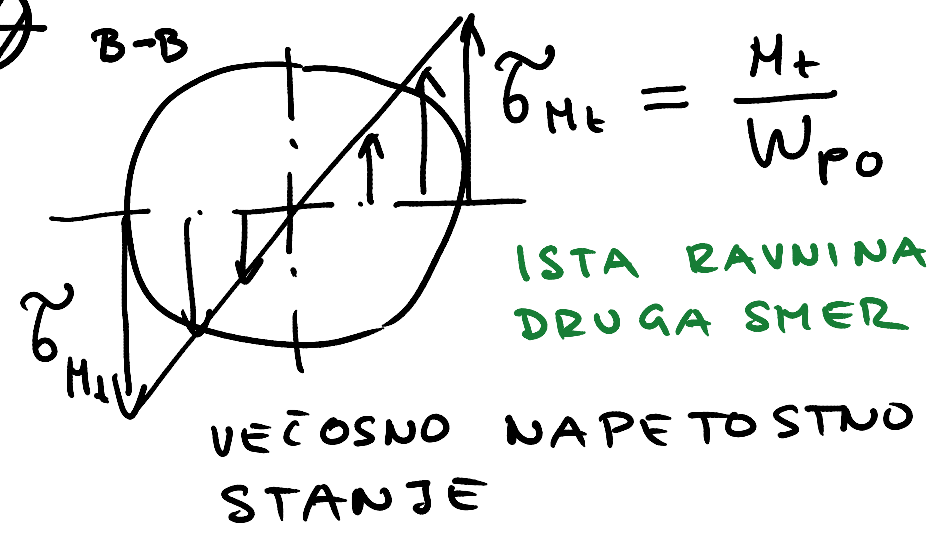
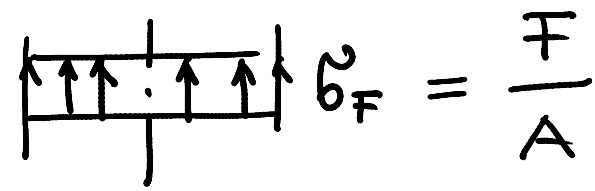
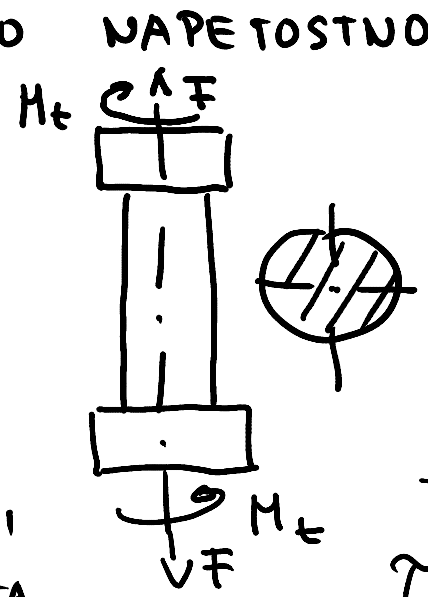
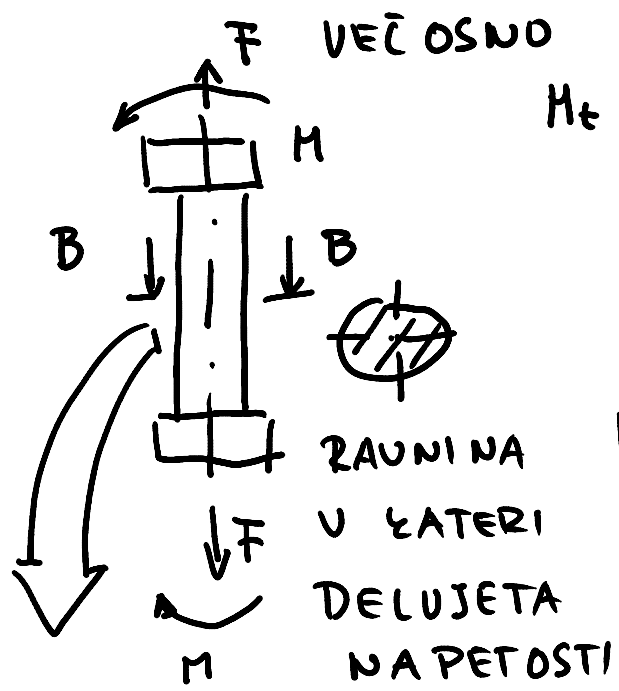
KUMULATIVNA FUNKCIJA
VERJETNOSTI



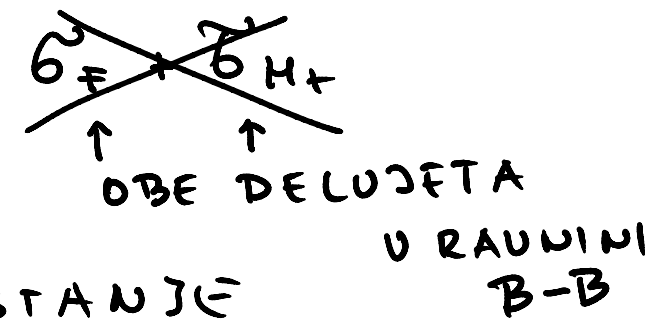
RAZTROS MERIMO S STANDARDNO DEVIACIJO σ_m

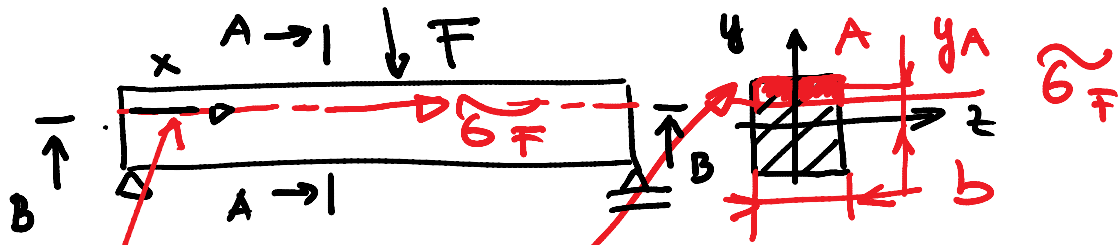
$$\sigma_m = \sqrt{\frac{1}{n} \sum_{i=1}^n (R_{mi} - \bar{R}_m)^2}$$





ISTA SMER ISTA RAUNINA
 $\sigma_F + \sigma_M = \sigma$ ENOSNO NAP. STANJE





$$T = \frac{F}{2}$$

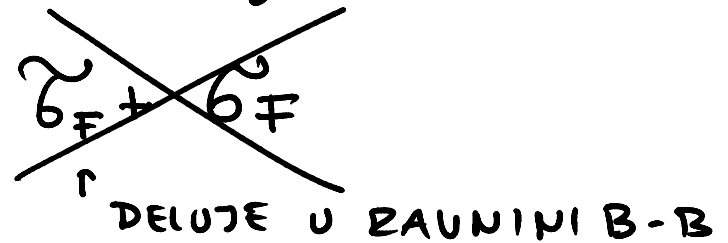
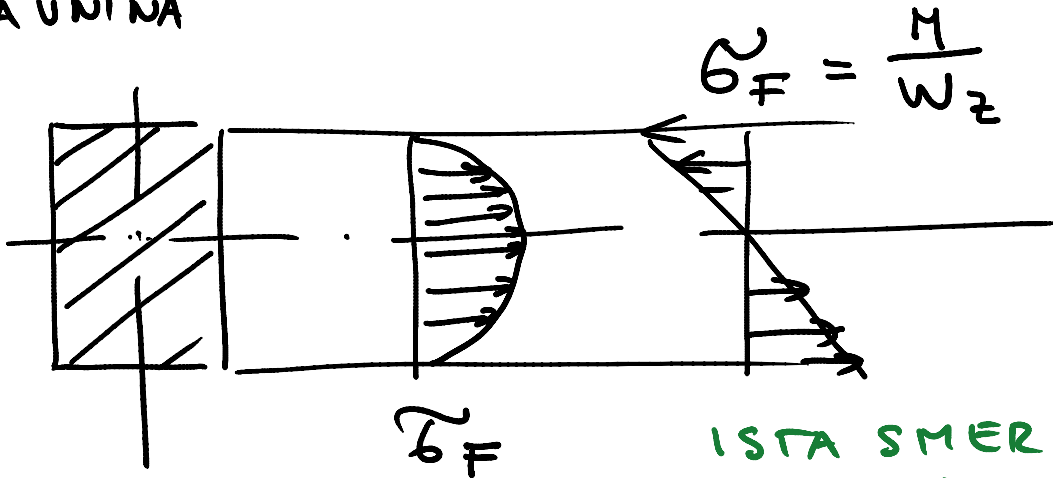
$$\tau_F = \frac{T \cdot S}{I_z \cdot b}$$

STATIČNI MOMENT PREREZA

$$S = A \cdot y_A$$

RAVNINA

DELOJE U RAVNINI A-A



ISTA SMER DRUGA RAVNINA

$$\sigma_x = \sigma; \tau_{xy} = \tau; \text{OSTALO } \emptyset$$

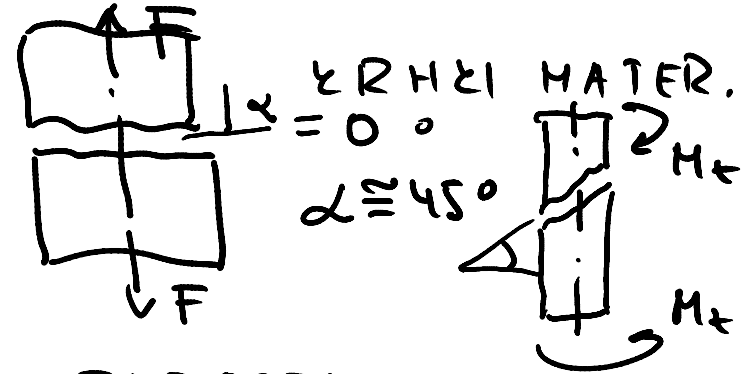
$$\sigma_{ij} = \begin{pmatrix} \sigma_x & \tau_{xy} & \tau_{xz} \\ \tau_{yx} & \sigma_y & \tau_{yz} \\ \tau_{zx} & \tau_{zy} & \sigma_z \end{pmatrix}$$

HIPOTEZA NAJVEĆJIH NORMALNIH NAPETOSTI

$$\sigma_v = \frac{1}{2} (\sigma + \sqrt{\sigma^2 + 4\tau^2})$$

$$\sigma = \phi \Rightarrow \sigma_v = \sigma$$

$$\tau = \phi \Rightarrow \sigma_v = \sigma$$

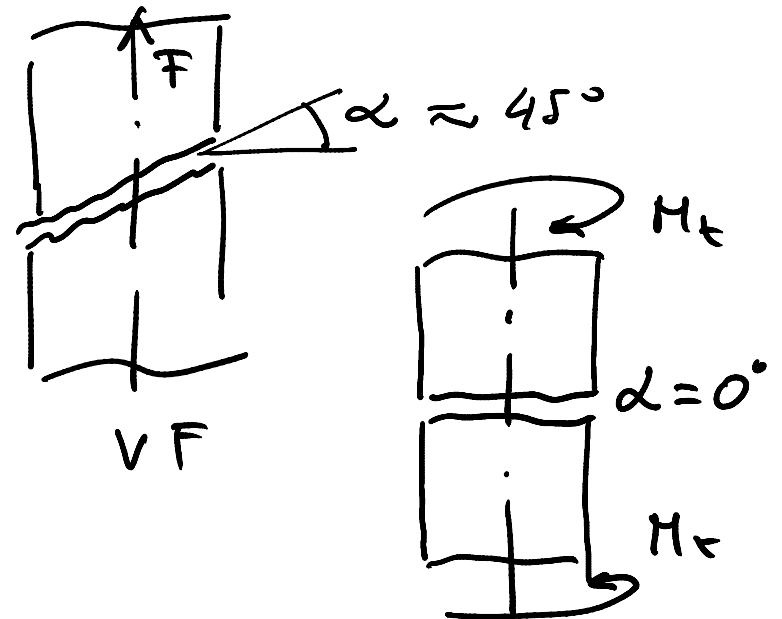


HIPOTEZA NAJVEĆJIH STRIŽNIH NAPETOSTI

$$\sigma_v = \sqrt{\sigma^2 + 4\tau^2} \quad \text{TRESKA}$$

$$\sigma = \phi \Rightarrow \sigma_v = 2\tau$$

$$\tau = \phi \Rightarrow \sigma_v = \sigma$$



ŽILAU MATERIAL

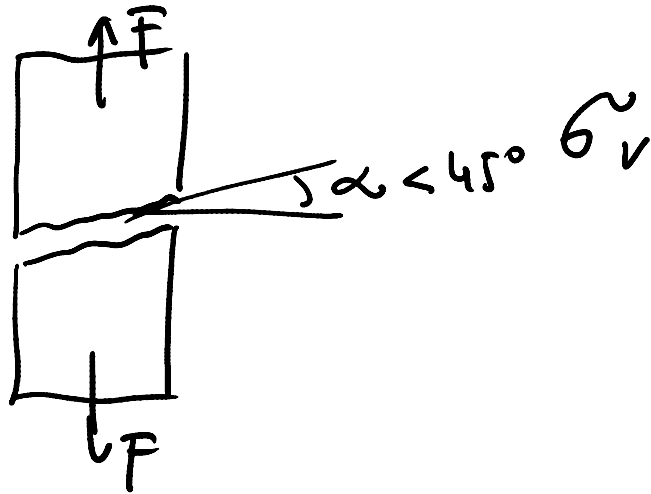
7 IZRAŽITO MEJO TEČENJA

HIPOTEZA NAJVEČJEGA PREGOBRAJNEGA DELA

$$\sigma_v = \sqrt{\sigma^2 + 3\tau^2}$$

$$\sigma = \phi \Rightarrow \sigma_v = \sqrt{3} \tau$$

$$\tau = \phi \Rightarrow \sigma_v = \sigma$$

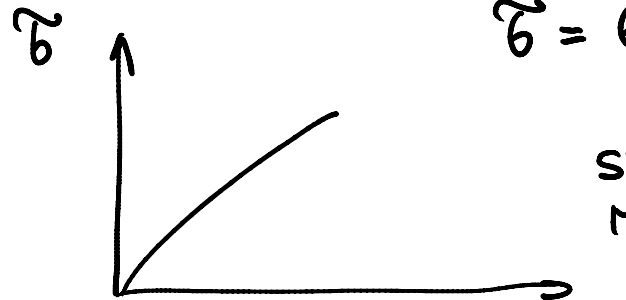


ŠILAU MAT.

Ž NEIŽRATITO MEJO TEČENJA

VON MISES-OVA HIPOTEZA

$$\leq \sigma_{dop}$$



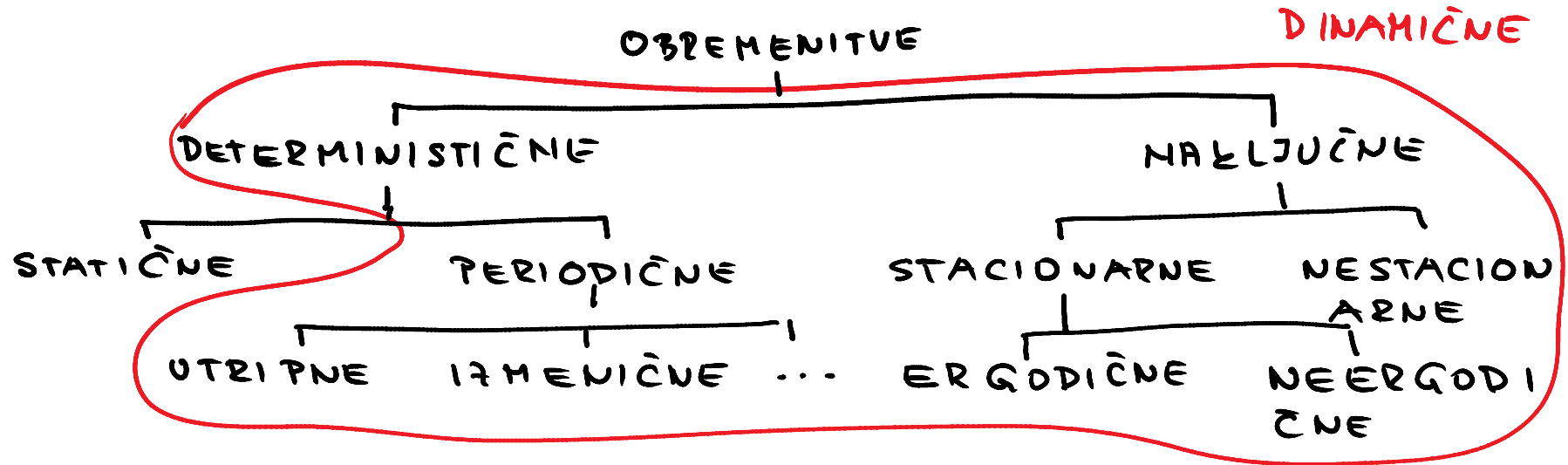
STRIŽNA SPECIFIČNA DEFORMACIJA

$$\tau = G \cdot \gamma$$

↑
STRIŽNI MODUL

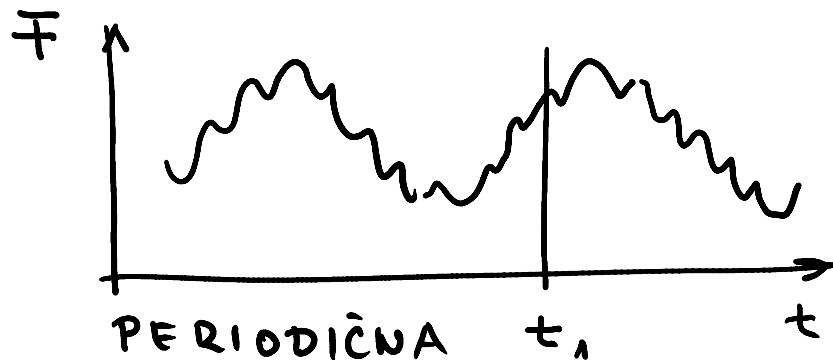
HODU TA KON γ
ZA STRIŽNE NAPETOSTI

URSTE OBREMENITEV



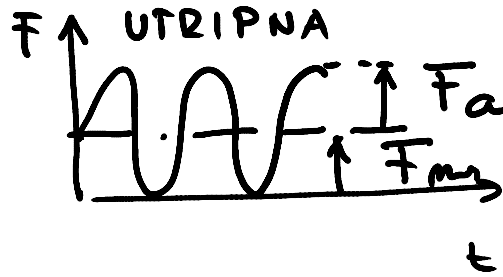
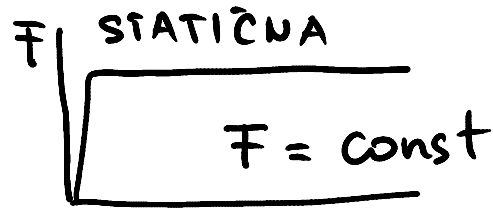
STATIČNE → ŽRHKI ALI PLASTIČNI LOM

DINAMIČNE → UTRUJENOSTNI LOM



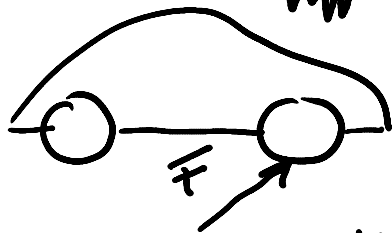
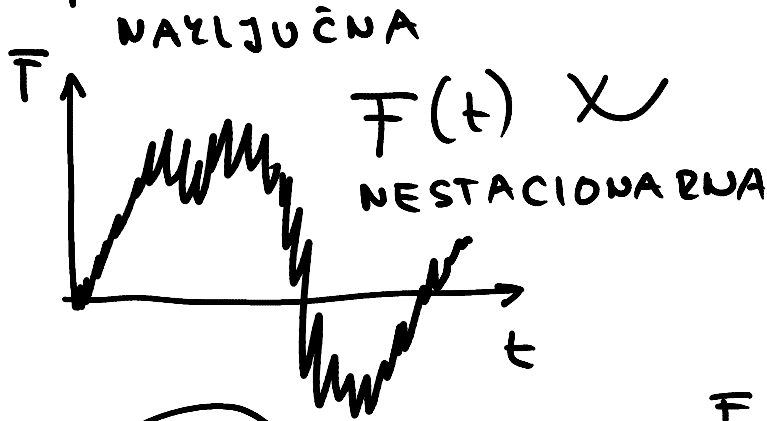
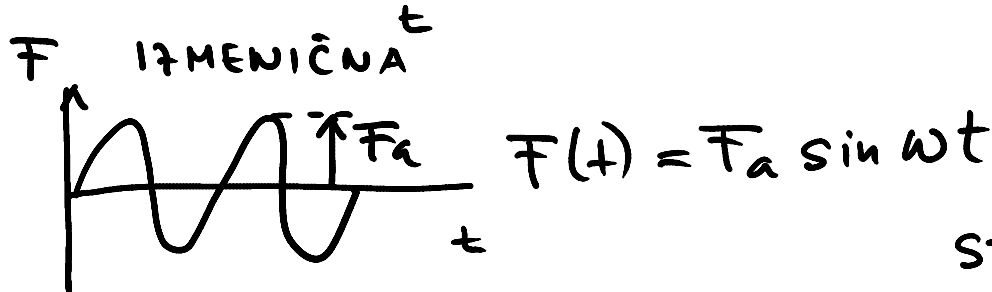
$$F(t_1) \checkmark$$

$$F(t) = A_1 \sin(\omega_1 t) + A_2 \cos \omega_2 t$$



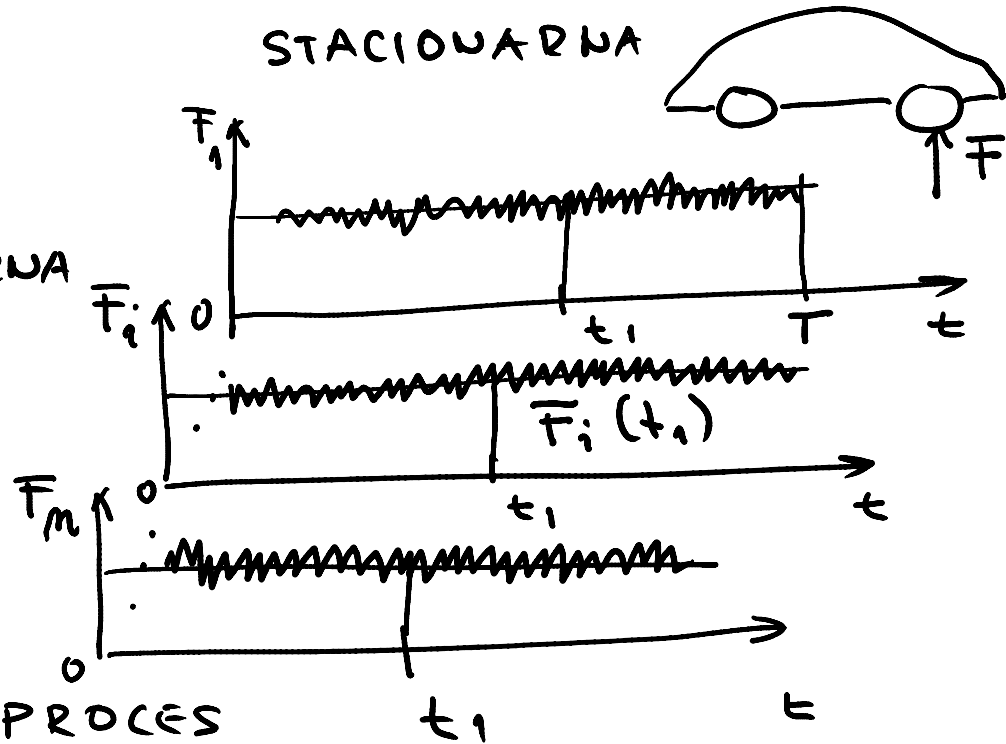
$$F(t) = F_m + F_a \sin \omega t$$

$$F_m = F_a$$



NAKLJUČNI PROCES

STACIONARNA

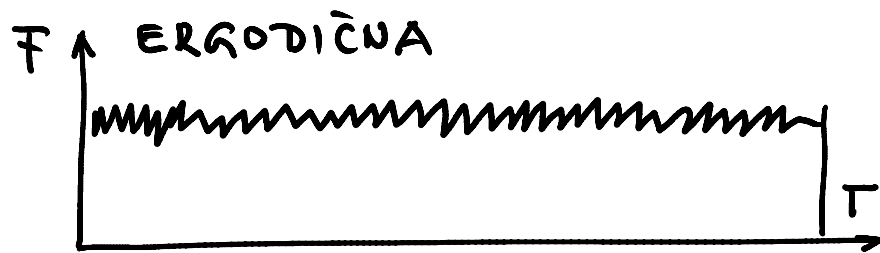


$$\bar{F}(t_1) = \lim_{n \rightarrow \infty} \frac{1}{n} \sum_{i=1}^n F_i(t_1) = M_1(t_1)$$

SREDNJA VREDNOST
PRVI MOMENT

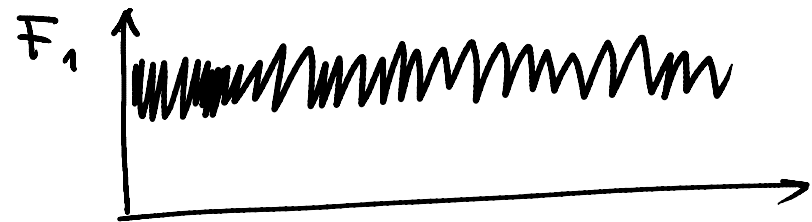
$$M_2(t_1) = \lim_{n \rightarrow \infty} \frac{1}{n} \sum_{i=1}^n F_i^2(t_1)$$

DRUGI MOMENT
DATE INFORMACIJO O
RAZTROSU OBREHENITVE



$$\bar{F} = \lim_{T \rightarrow \infty} \frac{1}{T} \int_0^T F(t) dt = M_1$$

$$M_2 = \lim_{T \rightarrow \infty} \frac{1}{T} \int_0^T F^2(t) dt$$



$$M_2 F_1 > M_2 F \quad t$$

$$\bar{F}(t_1) = \bar{F}(t_2) = \dots$$

ERGODIČNA OBREHENITEU

$$M_2(t_1) = M_2(t_2) = \dots$$

F

NEERGODIČNA

